

Isolated Footing Design(ACI 318-11)

Design For Isolated Footing 168

Design For Isolated Footing 170

Design For Isolated Footing 172

Design For Isolated Footing 174

Design For Isolated Footing 176

Design For Isolated Footing 178

Design For Isolated Footing 180

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Design For Isolated Footing 201

Design For Isolated Footing 203

Design For Isolated Footing 205

Design For Isolated Footing 207

Design For Isolated Footing 209

Design For Isolated Footing 211

Footing No.	Group ID	Foundation Geometry		
-	-	Length	Width	Thickness
168	1	1.630m	1.630m	0.300m

Footing No.	Footing Reinforcement				Pedestal Reinforcement	
-	Bottom Reinforcement(M ₂)	Bottom Reinforcement(M _x)	Top Reinforcement(M ₂)	Top Reinforcement(M _x)	Main Steel	Trans Steel
168	# 12 @ 16 cm c/c	# 12 @ 21 cm c/c	# 12 @ 21 cm c/c	# 12 @ 21 cm c/c	N/A	N/A

Footing No.	Group ID	Foundation Geometry		
-	-	Length	Width	Thickness
170	2	1.600m	1.600m	0.300m

Footing No.	Footing Reinforcement				Pedestal Reinforcement	
-	Bottom Reinforcement(M ₂)	Bottom Reinforcement(M _x)	Top Reinforcement(M ₂)	Top Reinforcement(M _x)	Main Steel	Trans Steel
170	# 12 @ 21 cm c/c	# 12 @ 21 cm c/c	# 12 @ 21 cm c/c	# 12 @ 21 cm c/c	N/A	N/A

Footing No.	Group ID	Foundation Geometry		
-	-	Length	Width	Thickness
172	3	1.820m	1.820m	0.350m

Footing No.	Footing Reinforcement				Pedestal Reinforcement	
-	Bottom Reinforcement(M ₂)	Bottom Reinforcement(M _x)	Top Reinforcement(M ₂)	Top Reinforcement(M _x)	Main Steel	Trans Steel
172	# 12 @ 15 cm c/c	# 12 @ 17 cm c/c	# 16 @ 33 cm c/c	# 16 @ 33 cm c/c	N/A	N/A

Footing No.	Group ID	Foundation Geometry		
-	-	Length	Width	Thickness
174	4	1.550m	1.550m	0.300m

Footing No.	Footing Reinforcement				Pedestal Reinforcement	
-	Bottom Reinforcement(M ₂)	Bottom Reinforcement(M _x)	Top Reinforcement(M ₂)	Top Reinforcement(M _x)	Main Steel	Trans Steel
174	# 12 @ 20 cm c/c	# 12 @ 20 cm c/c	# 12 @ 20 cm c/c	# 12 @ 20 cm c/c	N/A	N/A

Footing No.	Group ID	Foundation Geometry		
-	-	Length	Width	Thickness
176	5	1.660m	1.660m	0.300m

Footing No.	Footing Reinforcement				Pedestal Reinforcement	
-	Bottom Reinforcement(M ₂)	Bottom Reinforcement(M _x)	Top Reinforcement(M ₂)	Top Reinforcement(M _x)	Main Steel	Trans Steel
176	# 12 @ 17 cm c/c	# 16 @ 37 cm c/c	# 12 @ 21 cm c/c	# 12 @ 21 cm c/c	N/A	N/A

Footing No.	Group ID	Foundation Geometry		
-	-	Length	Width	Thickness
178	6	1.720m	1.720m	0.320m

Footing No.	Footing Reinforcement				Pedestal Reinforcement	
-	Bottom Reinforcement(M ₂)	Bottom Reinforcement(M _x)	Top Reinforcement(M ₂)	Top Reinforcement(M _x)	Main Steel	Trans Steel
178	# 12 @ 17 cm c/c	# 12 @ 17 cm c/c	# 16 @ 39 cm c/c	# 16 @ 39 cm c/c	N/A	N/A

Footing No.	Group ID	Foundation Geometry		
-	-	Length	Width	Thickness
180	7	1.890m	1.890m	0.360m

Footing No.	Footing Reinforcement				Pedestal Reinforcement	
-	Bottom Reinforcement(M ₂)	Bottom Reinforcement(M _x)	Top Reinforcement(M ₂)	Top Reinforcement(M _x)	Main Steel	Trans Steel
180	# 16 @ 29 cm c/c	# 12 @ 16 cm c/c	# 12 @ 17 cm c/c	# 12 @ 17 cm c/c	N/A	N/A

Footing No.	Group ID	Foundation Geometry		
-	-	Length	Width	Thickness
182	8	1.650m	1.650m	0.300m

Footing No.	Footing Reinforcement				Pedestal Reinforcement	
-	Bottom Reinforcement(M ₂)	Bottom Reinforcement(M _x)	Top Reinforcement(M ₂)	Top Reinforcement(M _x)	Main Steel	Trans Steel
182	# 12 @ 21 cm c/c	# 12 @ 21 cm c/c	# 12 @ 21 cm c/c	# 12 @ 21 cm c/c	N/A	N/A

Footing No.	Group ID	Foundation Geometry		
-	-	Length	Width	Thickness
184	9	1.650m	1.650m	0.310m

Footing No.	Footing Reinforcement				Pedestal Reinforcement	
-	Bottom Reinforcement(M ₂)	Bottom Reinforcement(M _x)	Top Reinforcement(M ₂)	Top Reinforcement(M _x)	Main Steel	Trans Steel
184	# 16 @ 37 cm c/c	# 16 @ 37 cm c/c	# 20 @ 45 cm c/c	# 20 @ 45 cm c/c	N/A	N/A

Footing No.	Group ID	Foundation Geometry		
-	-	Length	Width	Thickness
186	10	1.710m	1.710m	0.320m

Footing No.	Footing Reinforcement				Pedestal Reinforcement	
-	Bottom Reinforcement(M ₂)	Bottom Reinforcement(M _x)	Top Reinforcement(M ₂)	Top Reinforcement(M _x)	Main Steel	Trans Steel

186	# 16 @ 31 cm c/c	# 12 @ 17 cm c/c	# 16 @ 39 cm c/c	# 16 @ 39 cm c/c	N/A	N/A
Footing No.	Group ID		Foundation Geometry			
-	-		Length	Width	Thickness	
188	11		1.590m	1.590m	0.310m	
Footing No.	Footing Reinforcement				Pedestal Reinforcement	
-	Bottom Reinforcement(M ₂)	Bottom Reinforcement(M _x)	Top Reinforcement(M ₂)	Top Reinforcement(M _x)	Main Steel	Trans Steel
188	# 12 @ 16 cm c/c	# 12 @ 20 cm c/c	# 12 @ 20 cm c/c	# 12 @ 20 cm c/c	N/A	N/A
Footing No.	Group ID		Foundation Geometry			
-	-		Length	Width	Thickness	
190	12		1.550m	1.550m	0.300m	
Footing No.	Footing Reinforcement				Pedestal Reinforcement	
-	Bottom Reinforcement(M ₂)	Bottom Reinforcement(M _x)	Top Reinforcement(M ₂)	Top Reinforcement(M _x)	Main Steel	Trans Steel
190	# 12 @ 15 cm c/c	# 12 @ 20 cm c/c	# 12 @ 20 cm c/c	# 12 @ 20 cm c/c	N/A	N/A
Footing No.	Group ID		Foundation Geometry			
-	-		Length	Width	Thickness	
192	13		1.780m	1.780m	0.360m	
Footing No.	Footing Reinforcement				Pedestal Reinforcement	
-	Bottom Reinforcement(M ₂)	Bottom Reinforcement(M _x)	Top Reinforcement(M ₂)	Top Reinforcement(M _x)	Main Steel	Trans Steel
192	# 16 @ 27 cm c/c	# 16 @ 32 cm c/c	# 16 @ 32 cm c/c	# 16 @ 32 cm c/c	N/A	N/A
Footing No.	Group ID		Foundation Geometry			
-	-		Length	Width	Thickness	
193	14		1.520m	1.520m	0.300m	
Footing No.	Footing Reinforcement				Pedestal Reinforcement	
-	Bottom Reinforcement(M ₂)	Bottom Reinforcement(M _x)	Top Reinforcement(M ₂)	Top Reinforcement(M _x)	Main Steel	Trans Steel
193	# 12 @ 19 cm c/c	# 12 @ 19 cm c/c	# 12 @ 19 cm c/c	# 12 @ 19 cm c/c	N/A	N/A
Footing No.	Group ID		Foundation Geometry			
-	-		Length	Width	Thickness	
195	15		1.840m	1.840m	0.340m	
Footing No.	Footing Reinforcement				Pedestal Reinforcement	
-	Bottom Reinforcement(M ₂)	Bottom Reinforcement(M _x)	Top Reinforcement(M ₂)	Top Reinforcement(M _x)	Main Steel	Trans Steel
195	# 16 @ 28 cm c/c	# 12 @ 15 cm c/c	# 12 @ 19 cm c/c	# 12 @ 19 cm c/c	N/A	N/A
Footing No.	Group ID		Foundation Geometry			
-	-		Length	Width	Thickness	
197	16		1.640m	1.640m	0.300m	
Footing No.	Footing Reinforcement				Pedestal Reinforcement	
-	Bottom Reinforcement(M ₂)	Bottom Reinforcement(M _x)	Top Reinforcement(M ₂)	Top Reinforcement(M _x)	Main Steel	Trans Steel
197	# 16 @ 37 cm c/c	# 12 @ 21 cm c/c	# 12 @ 21 cm c/c	# 12 @ 21 cm c/c	N/A	N/A
Footing No.	Group ID		Foundation Geometry			
-	-		Length	Width	Thickness	
199	17		1.630m	1.630m	0.310m	
Footing No.	Footing Reinforcement				Pedestal Reinforcement	
-	Bottom Reinforcement(M ₂)	Bottom Reinforcement(M _x)	Top Reinforcement(M ₂)	Top Reinforcement(M _x)	Main Steel	Trans Steel
199	# 12 @ 16 cm c/c	# 16 @ 37 cm c/c	# 20 @ 45 cm c/c	# 20 @ 45 cm c/c	N/A	N/A
Footing No.	Group ID		Foundation Geometry			
-	-		Length	Width	Thickness	
201	18		1.700m	1.700m	0.320m	

Footing No.	Footing Reinforcement				Pedestal Reinforcement	
	Bottom Reinforcement(M _z)	Bottom Reinforcement(M _x)	Top Reinforcement(M _z)	Top Reinforcement(M _x)	Main Steel	Trans Steel
-						
201	# 12 @ 17 cm c/c	# 16 @ 38 cm c/c	# 16 @ 38 cm c/c	# 16 @ 38 cm c/c	N/A	N/A

Footing No.	Group ID	Foundation Geometry		
-	-	Length	Width	Thickness
203	19	1.530m	1.530m	0.300m

Footing No.	Footing Reinforcement				Pedestal Reinforcement	
	Bottom Reinforcement(M _z)	Bottom Reinforcement(M _x)	Top Reinforcement(M _z)	Top Reinforcement(M _x)	Main Steel	Trans Steel
-						
203	# 12 @ 20 cm c/c	# 12 @ 20 cm c/c	# 12 @ 20 cm c/c	# 12 @ 20 cm c/c	N/A	N/A

Footing No.	Group ID	Foundation Geometry		
-	-	Length	Width	Thickness
205	20	1.690m	1.690m	0.310m

Footing No.	Footing Reinforcement				Pedestal Reinforcement	
	Bottom Reinforcement(M _z)	Bottom Reinforcement(M _x)	Top Reinforcement(M _z)	Top Reinforcement(M _x)	Main Steel	Trans Steel
-						
205	# 12 @ 19 cm c/c	# 16 @ 38 cm c/c	# 16 @ 38 cm c/c	# 16 @ 38 cm c/c	N/A	N/A

Footing No.	Group ID	Foundation Geometry		
-	-	Length	Width	Thickness
207	21	1.630m	1.630m	0.310m

Footing No.	Footing Reinforcement				Pedestal Reinforcement	
	Bottom Reinforcement(M _z)	Bottom Reinforcement(M _x)	Top Reinforcement(M _z)	Top Reinforcement(M _x)	Main Steel	Trans Steel
-						
207	# 16 @ 37 cm c/c	# 16 @ 37 cm c/c	# 20 @ 45 cm c/c	# 20 @ 45 cm c/c	N/A	N/A

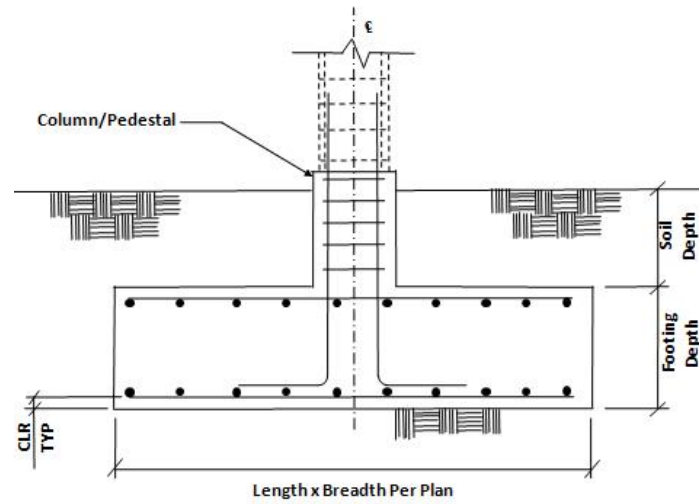
Footing No.	Group ID	Foundation Geometry		
-	-	Length	Width	Thickness
209	22	1.680m	1.680m	0.310m

Footing No.	Footing Reinforcement				Pedestal Reinforcement	
	Bottom Reinforcement(M _z)	Bottom Reinforcement(M _x)	Top Reinforcement(M _z)	Top Reinforcement(M _x)	Main Steel	Trans Steel
-						
209	# 12 @ 17 cm c/c	# 16 @ 38 cm c/c	# 20 @ 45 cm c/c	# 20 @ 45 cm c/c	N/A	N/A

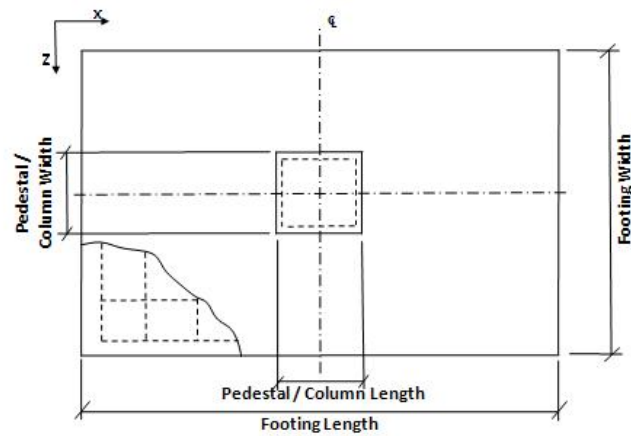
Footing No.	Group ID	Foundation Geometry		
-	-	Length	Width	Thickness
211	23	1.750m	1.750m	0.330m

Footing No.	Footing Reinforcement				Pedestal Reinforcement	
	Bottom Reinforcement(M _z)	Bottom Reinforcement(M _x)	Top Reinforcement(M _z)	Top Reinforcement(M _x)	Main Steel	Trans Steel
-						
211	# 16 @ 32 cm c/c	# 12 @ 18 cm c/c	# 12 @ 18 cm c/c	# 12 @ 18 cm c/c	N/A	N/A

Isolated Footing 168



ELEVATION



PLAN

[Input Values](#)

[Footing Geomtery](#)

Design Type : Calculate Dimension

Footing Thickness (Ft) : 300.000mm

Footing Length - X (Fl) : 1000.000mm

Footing Width - Z (Fw) : 1000.000mm

Eccentricity along X (Oxd) : 0.000mm

Eccentricity along Z (Ozd) : 0.000mm

[Column Dimensions](#)

Column Shape : Rectangular

Column Length - X (D_{col}) : 0.400m

Column Width - Z (B_{col}) : 0.400m

[Pedestal](#)

Include Pedestal? No
 Pedestal Shape : N/A
 Pedestal Height (Ph) : N/A
 Pedestal Length - X (Pl) : N/A
 Pedestal Width - Z (Pw) : N/A

Design Parameters

Concrete and Rebar Properties

Unit Weight of Concrete : 24.000kN/m3
 Strength of Concrete : 21.000N/mm2
 Yield Strength of Steel : 420.000N/mm2
 Minimum Bar Size : # 12
 Maximum Bar Size : # 20
 Pedestal Minimum Bar Size : 8
 Pedestal Maximum Bar Size : 9
 Minimum Bar Spacing : 50.000mm
 Maximum Bar Spacing : 450.000mm
 Pedestal Clear Cover (P, CL) : 75.000mm
 Footing Clear Cover (F, CL) : 75.000mm

Soil Properties

Soil Type : Drained
 Unit Weight : 19.000kN/m3
 Soil Bearing Capacity : 281.200kN/m2
 Soil Bearing Capacity Type: Gross Bearing Capacity
 Soil Surcharge : 0.000kN/m2
 Depth of Soil above Footing : 2.000m
 Cohesion : 0.000kN/m2

Sliding and Overturning

Coefficient of Friction : 0.500
 Factor of Safety Against Sliding : 1.500
 Factor of Safety Against Overturning : 1.500

Design Calculations

Footing Size

Initial Length (L_o) = 1.000m
 Initial Width (W_o) = 1.000m

Load Combination/ s- Service Stress Level				
Load		Load	Soil	Self

Combination Number	Load Combination Title	Combination Factor	Bearing Factor	Weight Factor
22	CM + CV	1.00	1.00	1.00
23	CM + 0,75 CV + 0.75 (0.7)(SX + 0,3 SZ)/R	1.00	1.00	1.00
24	CM + 0,75 CV - 0.75 (0.7)(SX - 0,3 SZ)/R	1.00	1.00	1.00
25	CM + 0,75 CV + 0.75 (0.7)(SX - 0,3 SZ)/R	1.00	1.00	1.00
26	CM + 0,75 CV - 0.75 (0.7)(SX + 0,3 SZ)/R	1.00	1.00	1.00
27	CM + 0,75 CV + 0.75 (0.7)(0,3 SX + SZ)/R	1.00	1.00	1.00
28	CM + 0,75 CV - 0.75 (0.7)(0,3 SX - SZ)/R	1.00	1.00	1.00
29	CM + 0,75 CV + 0.75 (0.7)(0,3 SX - SZ)/R	1.00	1.00	1.00
30	CM + 0,75 CV - 0.75 (0.7)(0,3 SX + SZ)/R	1.00	1.00	1.00
31	0.6 CM + 0.700 (SX + 0.3 SZ)/R	1.00	1.00	1.00
32	0.6 CM - 0.700 (SX - 0.3 SZ)/R	1.00	1.00	1.00
33	0.6 CM + 0.700 (SX - 0.3 SZ)/R	1.00	1.00	1.00
34	0.6 CM - 0.700 (SX + 0.3 SZ)/R	1.00	1.00	1.00
35	0.6 CM + 0.700 (0.3 SX + SZ)/R	1.00	1.00	1.00
36	0.6 CM - 0.700 (0.3 SX - SZ)/R	1.00	1.00	1.00
37	0.6 CM - 0.700 (0.3 SX + SZ)/R	1.00	1.00	1.00
38	0.6 CM + 0.700 (0.3 SX - SZ)/R	1.00	1.00	1.00

Load Combination Number	Load Combination Title	Load Combination Factor	Soil Bearing Factor	Self Weight Factor
5	1.2 CM + 1.600 CV	1.00	1.00	1.00
6	1.2 CM + CV + (SX/R + 0,30 SZ/R)	1.00	1.00	1.00
7	1.2 CM + CV - (SX/R - 0,30 SZ/R)	1.00	1.00	1.00
8	1.2 CM + CV + (SX/R - 0,30 SZ/R)	1.00	1.00	1.00
9	1.2 CM + CV - (SX/R + 0,30 SZ/R)	1.00	1.00	1.00
10	1.2 CM + CV + (0.3 SX/R + SZ/R)	1.00	1.00	1.00
11	1.2 CM + CV - (0.3 SX/R - SZ/R)	1.00	1.00	1.00
12	1.2 CM + CV + (0.3 SX/R - SZ/R)	1.00	1.00	1.00
13	1.2 CM + CV - (0.3 SX/R + SZ/R)	1.00	1.00	1.00
14	0.9 CM + (SX/R + 0,30 SZ/R)	1.00	1.00	1.00
15	0.9 CM - (SX/R - 0,30 SZ/R)	1.00	1.00	1.00
16	0.9 CM + (SX/R - 0,30 SZ/R)	1.00	1.00	1.00
17	0.9 CM - (SX/R + 0,30 SZ/R)	1.00	1.00	1.00
18	0.9 CM + (0.3 SX/R + SZ/R)	1.00	1.00	1.00
19	0.9 CM - (0.3 SX/R - SZ/R)	1.00	1.00	1.00
20	0.9 CM + (0.3 SX/R - SZ/R)	1.00	1.00	1.00
21	0.9 CM - (0.3 SX/R + SZ/R)	1.00	1.00	1.00

Applied Loads - Service Stress Level					
LC	Axial (kN)	Shear X (kN)	Shear Z (kN)	Moment X (kNm)	Moment Z (kNm)
22	330.840	-0.193	-10.635	-11.480	1.545
23	298.842	19.573	-2.978	4.562	-40.862
24	335.403	-19.004	-9.097	-8.706	42.406
25	307.175	19.172	-10.967	-12.921	-40.002
26	343.736	-19.404	-17.086	-26.188	43.266
27	300.345	6.598	5.720	23.639	-12.850
28	312.830	-5.016	2.406	16.423	12.219
29	329.748	5.185	-22.469	-38.050	-9.814
30	340.686	-6.355	-24.300	-42.019	15.095
31	145.612	26.537	4.509	15.295	-55.985
32	194.361	-24.899	-3.650	-2.395	55.039

33	156.802	25.999	-6.219	-8.182	-54.829
34	205.551	-25.437	-14.377	-25.872	56.194
35	149.668	9.192	14.098	36.338	-18.537
36	164.355	-6.305	11.640	31.008	14.912
37	201.496	-8.091	-23.967	-46.915	18.747
38	186.809	7.406	-21.509	-41.585	-14.703

Applied Loads - Strength Level					
LC	Axial (kN)	Shear X (kN)	Shear Z (kN)	Moment X (kNm)	Moment Z (kNm)
5	412.290	-0.676	-13.726	-14.842	2.402
6	346.705	36.972	1.172	16.078	-78.241
7	416.078	-36.225	-10.438	-9.096	79.753
8	362.657	36.205	-14.120	-17.389	-76.594
9	432.030	-36.992	-25.731	-42.563	81.400
10	352.472	12.306	14.809	46.001	-24.991
11	373.409	-9.785	11.304	38.404	22.693
12	405.326	9.765	-35.863	-64.889	-19.534
13	426.263	-12.326	-39.367	-72.486	28.150
14	220.710	37.808	6.050	21.388	-79.664
15	290.083	-35.390	-5.560	-3.786	78.331
16	236.662	37.041	-9.242	-12.079	-78.017
17	306.035	-36.157	-20.853	-37.253	79.978
18	226.477	13.142	19.687	51.311	-26.413
19	247.414	-8.949	16.182	43.714	21.270
20	279.331	10.600	-30.985	-59.579	-20.956
21	300.268	-11.491	-34.489	-67.176	26.727

Reduction of force due to buoyancy = 0.000kN

Effect due to adhesion = 0.000kN

Area from initial length and width, $A_o = L_o \times W_o = 1.000\text{m}^2$

Min. area required from bearing pressure, $A_{\min} = P / q_{\max} = 1.344\text{m}^2$

Note: A_{\min} is an initial estimation.

P = Critical Factored Axial Load(without self weight/ buoyancy/ soil).

q_{\max} = Respective Factored Bearing Capacity.

Final Footing Size

Length (L_2) = 1.630 m Governing Load Case : # 26

Width (W_2) = 1.630 m Governing Load Case : # 26

Depth (D_2) = 0.300 m Governing Load Case : # 13

Depth is governed by Ultimate Load Case

(Service check is performed with footing thickness requirements from concrete check)

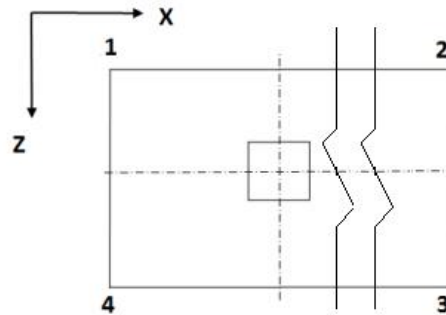
Area (A_2) = 2.657 m^2

Final Soil Height = 1.700 m

Footing Self Weight = 19.129 kN

Soil Weight On Top Of Footing
= 80.647 kN

Pressures at Four Corners



Load Case	Pressure at corner 1 (q_1) (kN/ m2)	Pressure at corner 2 (q_2) (kN/ m2)	Pressure at corner 3 (q_3) (kN/ m2)	Pressure at corner 4 (q_4) (kN/ m2)	Area of footing in uplift (A_u) (m ²)
26	278.3218	142.3042	55.5353	191.5529	0.000
29	207.9670	239.4722	115.3605	83.8554	0.000
23	80.2008	209.6968	219.8617	90.3657	0.000
24	246.2849	112.9843	81.2995	214.6001	0.000

If A_u is zero, there is no uplift and no pressure adjustment is necessary. Otherwise, to account for uplift, areas of negative pressure will be set to zero and the pressure will be redistributed to remaining corners.

Summary of Adjusted Pressures at 4 corners Four Corners

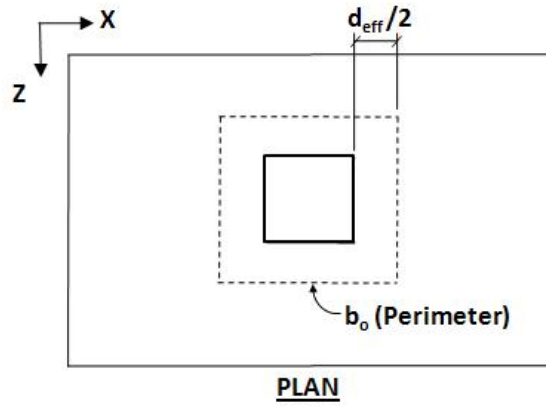
Load Case	Pressure at corner 1 (q_1) (kN/ m2)	Pressure at corner 2 (q_2) (kN/ m2)	Pressure at corner 3 (q_3) (kN/ m2)	Pressure at corner 4 (q_4) (kN/ m2)
26	278.3218	142.3042	55.5353	191.5529
29	207.9670	239.4722	115.3605	83.8554
23	80.2008	209.6968	219.8617	90.3657
24	246.2849	112.9843	81.2995	214.6001

Compression Development Length Check

Development length skipped as column reinforcement is not specified in input (Column Dimnesion Task Pane)

Shear Calculation

Punching Shear Check



Total Footing Depth, $D = 0.300\text{m}$
 Calculated Effective Depth, $d_{\text{eff}} = D - C_{\text{cover}} - 0.5 \cdot d_b = 0.219\text{m}$
 For rectangular column, $\beta_c = B_{\text{col}} / D_{\text{col}} = 1.000$

Effective depth, d_{eff} , increased until $0.75XV_c \geq$ Punching Shear Force

Punching Shear Force, $V_u = 455.112\text{kN}$, Load Case # 9

From ACI Cl.11.11.2, b_o for column = $2 \times (B_{\text{col}} + D_{\text{col}} + 2 \times d_{\text{eff}}) = 2.476\text{m}$

Equation 11-31, $V_{c1} = \left(2 + \frac{4}{\beta_c}\right) \times b_o \times d_{\text{eff}} \times \sqrt{1000 \times F_c'} = 1237.985\text{kN}$

Equation 11-32, $V_{c2} = \left(2 + 40 \times \frac{d_{\text{eff}}}{b_o}\right) \times b_o \times d_{\text{eff}} \times \sqrt{1000 \times F_c'} = 1142.652\text{kN}$

Equation 11-33, $V_{c3} = 4 \times b_o \times d_{\text{eff}} \times \sqrt{1000 \times F_c'} = 825.323\text{kN}$

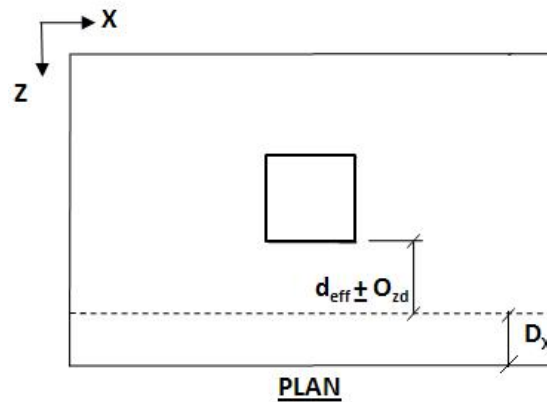
Punching shear strength, $V_c = 0.75 \times \text{minimum of } (V_{c1}, V_{c2}, V_{c3}) = 618.992\text{kN}$

$0.75 \times V_c > V_u$ hence, OK

One-Way Shear Check

Along X Direction

(Shear Plane Parallel to Global X Axis)



From ACI Cl.11.2.1.1, $V_c = 2 \times L \times d_{\text{eff}} \times \sqrt{1000 \times F_c'} = 271.663\text{kN}$

Distance along X to design for shear,
 $D_x = 0.5 \times (W - D_{col}) - d_{eff} + O_{zd} = 0.396 \text{ m}$

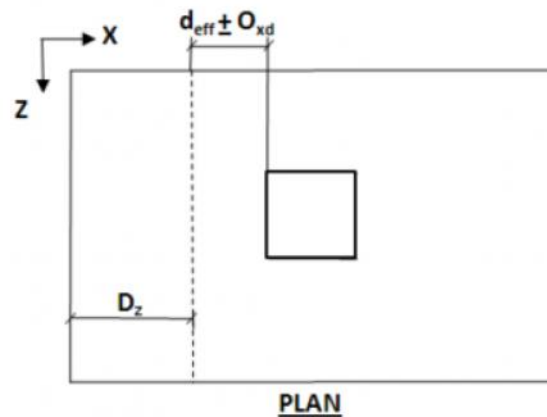
Check that $0.75 \times V_c > V_{ux}$ where V_{ux} is the shear force for the critical load cases at a distance d_{eff} from the face of the column caused by bending about the X axis.

From above calculations, $0.75 \times V_c = 203.747 \text{ kN}$
 Critical load case for V_{ux} is # 13 $V_{ux} = V_{ux}|_{x=D_x} = 184.869 \text{ kN}$
 $0.75 \times V_c > V_{ux}$ hence, OK

One-Way Shear Check

Along Z Direction

(Shear Plane Parallel to Global Z Axis)



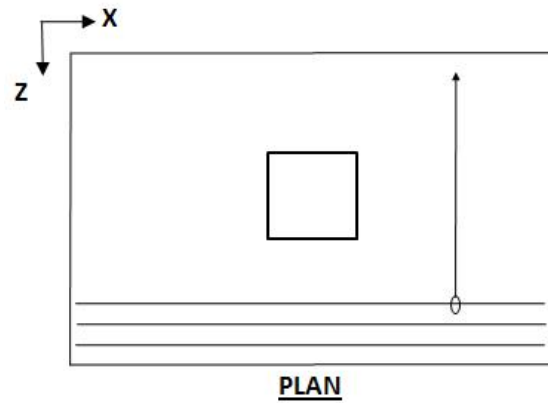
From ACI Cl.11.2.1.1, $V_c = 2 \times W \times d_{eff} \times \sqrt{1000 \times F_c'} = 271.663 \text{ kN}$
 Distance along X to design for shear, $D_z = 0.5 \times (L - B_{col}) - d_{eff} + O_{zd} = 0.396 \text{ m}$

Check that $0.75 \times V_c > V_{uz}$ where V_{uz} is the shear force for the critical load cases at a distance d_{eff} from the face of the column caused by bending about the Z axis.

From above calculations, $0.75 \times V_c = 203.747 \text{ kN}$
 Critical load case for V_{uz} is # 9 $V_{uz} = V_{uz}|_{z=D_z} = 191.823 \text{ kN}$
 $0.75 \times V_c > V_{uz}$ hence, OK

Design for Flexure about Z Axis

(For Reinforcement Parallel to X Axis)



Calculate the flexural reinforcement along the X direction of the footing. Find the area of steel required, A, as per Section 3.8 of Reinforced Concrete Design (5th ed.) by Salmon and Wang (Ref. 1)

Critical Load Case # 9

The strength values of steel and concrete used in the formulae are in ksi

Bars parallel to X Direction are placed at bottom

Effective Depth d_{eff} =		0.217 m
Factor β_1 from ACI Cl.10.2.7.3 =		0.850
From ACI Cl. 10.3.2, ρ_{bal} =	$0.85 \times \beta_1 \times F_c' \times \frac{87}{[f_y \times (87 + F_y)]}$	0.02125
From ACI Cl. 10.3.3, ρ_{max} =	$0.75 \times \rho_{bal}$	0.01594
From ACI Cl. 7.12.2, ρ_{min} =		0.00180
From Ref. 1, Eq. 3.8.4a, constant m =	$\frac{F_y}{(0.85 \times F_c')}$	23.529

Calculate reinforcement ratio ρ for critical load case

Design for flexure about Z axis is performed at the face of the column at a distance, D_x =	$0.5 \times L - 0.5 \times D_{col} + O_{xd}$	0.615 m
Ultimate moment,	$M_u _{z=D_x}$	91.258 kNm
Nominal moment capacity, M_n =	$\frac{M_u}{\phi}$	101.397 kNm
(Based on effective depth) Required ρ =	$\frac{1}{m} \times \left[1 - \sqrt{1 - 2 \times m \times \frac{M_n}{(F_y \times W \times d_{eff}^2)}} \right]$	0.00321
(Based on gross depth) $\rho \times d_{eff} / \text{Depth}$ =		0.00234
Since	$U_{min} \leq U \leq U_{max}$	OK
Area of Steel Required, A_s =	$\rho \times W \times d_{eff}$	1145.661 mm ²

Selected bar Size = # 16

Minimum spacing allowed (S_{min}) = 5.000cm

Selected spacing (S) = 29.280cm

$S_{\min} \leq S \leq S_{\max}$ and selected bar size < selected maximum bar size...

The reinforcement is accepted.

According to ACI 318 Clause No- 10.6.4

Max spacing for Cracking Consideration = 18.777cm

Warning: Calculated spacing is more than maximum spacing considering cracking condition. Modify spacing manually if cracking consideration is necessary.

Based on spacing reinforcement increment; provided reinforcement is

16 @ 20.500cm o.c.

$$\text{Required development length for bars} = \frac{0.87 \times d_b \times f_y}{4 \times \beta \times \sqrt{f_c}} = 0.305 \text{ m}$$

$$\text{Available development length for bars, } D_L = 0.5 \times (L - D_{\text{col}}) - C_{\text{cover}} = 0.540 \text{ m}$$

$$\text{Try bar size \# 16} \quad \text{Area of one bar} = 201.064 \text{ mm}^2$$

$$\text{Number of bars required, } N_{\text{bar}} = \frac{A_s}{A_{\text{bar}}} = 6$$

Because the number of bars is rounded up, make sure new reinforcement ratio < U_{\max}

$$\text{Total reinforcement area, } A_{s_{\text{total}}} = N_{\text{bar}} \times (\text{Area of one bar}) = 1206.385 \text{ mm}^2$$

$$d_{\text{eff}} = D - C_{\text{cover}} - 0.5 \times (\text{dia. of one bar}) = 0.217 \text{ m}$$

$$\text{Reinforcement ratio, } \rho = \frac{A_{s_{\text{total}}}}{(d_{\text{eff}} \times W)} = 0.00341$$

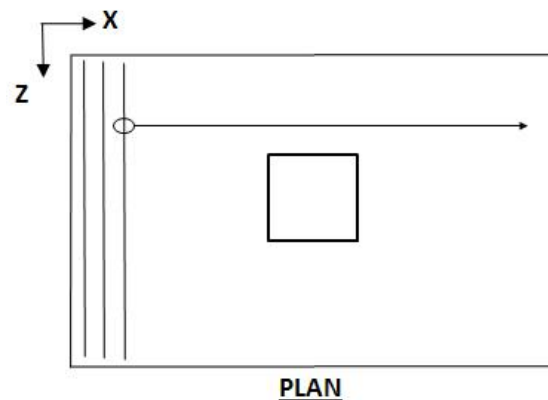
From ACI Cl.7.6.1, minimum req'd clear distance between bars

$$C_d = \max (\text{Diameter of one bar}, 1.0" (25.4\text{mm}), \text{Min. User Spacing}) = 5.000\text{cm}$$

Check to see if width is sufficient to accommodate bars

Design for Flexure about X axis

(For Reinforcement Parallel to Z Axis)



Calculate the flexural reinforcement along the Z direction of the footing. Find the area of steel required, A, as per Section 3.8 of Reinforced Concrete Design (5th ed.) by Salmon and Wang (Ref. 1)

Critical Load Case # 13

The strength values of steel and concrete used in the formulae are in ksi

Bars parallel to X Direction are placed at bottom

Effective Depth d_{eff} =		0.201 m
Factor β_1 from ACI Cl.10.2.7.3 =		0.850
From ACI Cl. 10.3.2, ρ_{bal} =	$0.85 \times \beta_1 \times F_c' \times \frac{87}{[F_y \times (87 + F_y)]}$	0.02125
From ACI Cl. 10.3.3, ρ_{max} =	$0.75 \times \rho_{bal}$	0.01594
From ACI Cl.7.12.2, ρ_{min} =		0.00180
From Ref. 1, Eq. 3.8.4a, constant m =	$\frac{F_y}{(0.85 \times F_c')}$	23.529

Calculate reinforcement ratio ρ for critical load case

Design for flexure about X axis is performed at the face of the column at a distance, D_z =	$0.5 \times L + 0.5 \times B_{col} + O_{zd}$	0.615 m
Ultimate moment, $M_u _{x=D_x}$ =		87.968 kNm
Nominal moment capacity, M_n =	$\frac{M_u}{\phi}$	97.742 kNm
(Based on effective depth) Required ρ =	$\frac{1}{m} \times \left[1 - \sqrt{1 - 2 \times m \times \frac{M_n}{(F_y \times W \times d_{eff}^2)}} \right]$	0.00347
(Based on gross depth) $\rho \times d_{eff}$ / Depth =		0.00240
Since $U_{min} \leq U \leq U_{max}$		OK
Area of Steel Required, A_s =	$\rho \times W \times d_{eff}$	1172.172 mm ²

Selected Bar Size = # 16

Minimum spacing allowed (S_{min}) = 5.000cm

Selected spacing (S) = 29.280cm

$S_{min} \leq S \leq S_{max}$ and selected bar size < selected maximum bar size...

The reinforcement is accepted.

According to ACI 318 Clause No- 10.6.4

Max spacing for Cracking Consideration = 18.777cm

Warning: Calculated spacing is more than maximum spacing considering cracking condition. Modify spacing manually if cracking consideration is necessary.

Based on spacing reinforcement increment; provided reinforcement is

16 @ 16.000cm o.c.

Required development length for bars = 0.305 m

$$\frac{0.87 \times d_b \times f_y}{4 \times \beta \times \sqrt{f_c}} =$$

Available development length for bars, D_L = $0.5 \times (L - D_{col}) - C_{cover} = 0.540 \text{ m}$

Try bar size # 16 Area of one bar = 201.064 mm²

Number of bars required, $N_{bar} = \frac{A_s}{A_{bar}} = 6$

Because the number of bars is rounded up, make sure new reinforcement ratio < U_{max}

Total reinforcement area, $A_{s_total} = N_{bar} \times (\text{Area of one bar}) = 1206.385 \text{ mm}^2$

$d_{eff} = D - C_{cover} - 1.5 \times (\text{dia. of one bar}) = 0.201 \text{ m}$

Reinforcement ratio, $\rho = \frac{A_{s_total}}{(d_{eff} \times W)} = 0.00368$

From ACI Cl.7.6.1, minimum req'd clear distance between bars

$C_d = \max (\text{Diameter of one bar}, 1.0" (25.4\text{mm}), \text{Min. User Spacing}) = 5.000\text{cm}$

Check to see if width is sufficient to accomodate bars

Isolated Footing 170